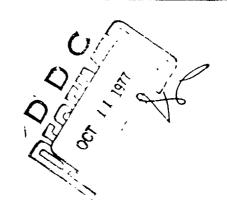
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TECHNICAL REPORT 7T-3-CEMEL

EVALUATION OF US AIR FORCE SURVIVAL/ARMOR VEST IN US ARMY OH-58 HELICOPTERS



Approved for public release; distribution unlimited.

FEBRUARY 1976

UNITED STATES ARMY
NATICK RESEARCH and DEVELOPMENT COMMAND
NATICK MASSACHUSETTS 01760



Clothing, Equipment and Materials Engineering Laboratory
CEMEL-161

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The Test Report, (Ref 1), found a number of flight safety hazards with both vests. However, the test report did not identify in detail the deficiencies found with the USAF Vest. This report identifies those conditions found on the OH-58 type Helicopter.

Four evaluations: Statiz, Flight, Body Load and Frezeurs, and Sizing were conducted and these revealed a number of minor design deficiencies. The material used in the vest construction does not provide sufficient retention of the armor insert and carrier. Lack of retigition caused the armor insert to rest on the pilots legs creating leg disconfert.

The USAF Survival/Armor Vest requires redesigning to correct the deficiencies presented here. The sizing criteria were also evaluated. New Sizing criteria are recommended to improve the sizing.

#### FOREWARD

This evaluation was conducted in coordination with the Tri Service Aircrew Body Armor Working Group. This report covers the work effort accomplished during 1975.

The USA NARADCOM Project Officer, Mr. Thomas H. Judge, was assisted in this evaluation at US Army Natick Research and Development Command and Ft. Devens Air Field by Capt. Paul Severance who served as a test subject and many members of the flight operation staff and maintenance crews at Ft. Devens Air Field. Mr. Fred Meers of USA NARADCOM photographed all the scenes for still and motion picture records.

The outstanding efforts of the above personnel contributed greatly to the success of this evaluation.

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#### SUMMARY

This evaluation revealed the US Air Force Survival/Armor Vest has a number of deficiencies that could be identified as Human Factor problems, contributing to incompatibilities between the pilot and his effort to satisfactorily operate the OH-58 Helicopter. The material used in the survival vest design does not provide for sufficient retention on the pilot's body of the armor carrier and insert during flight. The length of the armor insert and its side edges limit the pilot's ability to properly operate the controls of the Oh-58 Helicopter.

The deficiencies dited are minor design oblems. However, they do restrict the pilot's motion during flight and, as such, were listed as flight safety hazards. A modification program, such as a product improvement program, could be undertaken to modify the armor insert, armor carrier, and the survival vest to eliminate these problems. A Human Factors study would be required to determine the dimensional profile of the armor insert. Modification of the insert would then be required to meet a new profile outline. Action should also be taken to redesign the armor carrier to meet the new profile outline for the armor insert. This action would provide the opportunity to review and apply the latest state-of-the-art in ballistic fabric materials.

The survival vest will require redesigning to include weight retention characteristics to support the weight of the armor carrier and insert in a position on the body where it will not restrict the pilot's movements nor create physical discomfort.

A computer evaluation of the sizing criteria used for the USAF armor insert four-size system was conducted and indicated the criteria of using Stature, Waist, and Chest Circumference had a "No-Fit" percentage of 64.71. It was discovered that by using Vertical Trunk measurement in place of Stature, the "No-Fit" percentage drops to 22.23% and distributes the four sizes more evenly over the population. A Human Factors study is further indicated to evaluate the practical application of this change among USAF personnel and possible members of the US Army and US Navy Aviation Communities.

#### EVALUATION OF US AIR FORCE SURVIVAL/ARMOR VEST

#### IN US ARMY OH-58 HELICOPTERS

#### INTRODUCTION

The United States Air Force Survival/Armor Vest Concept, figure 1, which consists of a vest fabricated of nomex raschel knit, and back and front anatomical shaped caramic inserts contained in carriers of ballistic protective fabric and felt, was introduced into the Development Test II of the US Army Individual Survival Vest for Aircrewmembers as an intraservice standardization item for comparison review in US Army helicopters. The US Army Individual Survival Vest for Aircrewmembers, figure 2, is fabricated of nomex oxford cloth. It has pockets to contain the SRU-21/P Survival Vest component, back and front ceramic armor inserts covered with spall, and fragmentation carriers fabricated from ballistic protective fabric and felt.

Both Survival/Armor Vest concepts were designed to provide pockets to contain the standard survival components presently used in the Individual Survival Vest SRU-21/P and ceramic armor protective inserts to protect the aircrewmember from 30-caliber armor piercing projectiles. The US Army Aviation Test Board at Ft. Rucker, AL., following the completion of the test program, published a final report Development Test II (Service Phase) of the Individual Survival Vest for Aircrewmembers, citing a number of flight safety hazards caused by the US Army Individual Survival Vest for Aircrewmembers and further stated the same deficiences were found associated with the USAF Survival/Armor Vest Concept. The development program for US Army Individual Survival Vest for aircrewmembers was terminated following the Development Test II Program.

The flight safety deficiences cited in the final test report for the USAF Survival/Armor Vest concept were not defined in detail by the US Army Aviation Test Board. Therefore, under the Department of Defense Tri-Service Agreement on Aircrew Body Armor, 2 the US Army Natick Research and Development Command, as the lead laboratory for the refinement, design engineering, and development of aircrew body armor for interface with the USAF and US Navy embarked on an evaluation program to identify these deficiences in detail, using the USAF Survival/Armor Vest in the OH-58 US Army Helicopter. This helicopter was identified through analysis of the final test report (see ref. 1) to have the greatest number of problem areas. The identification of these deficiences permits this Command, in cooperation with the USAF, the opportunity to take corrective redesign actions to eliminate the flight safety hazards cited by the US Army Aviation Test Board against the present design.

Development Test II (Service Phase) of Individual Survival Vest for Aircrewmembers Oct 1974, Captain Leslie C. Mingus, Project Officer USAAVTED, AL.

<sup>3</sup>Joint Agreement on Consolidation of Functions and Facilities Aircrew Body Armor 29Mar1972

to achieve the objectives of this evaluation, four studies were undertaken to define and identify the pilot's areas and actions that lead to the safety of flight citations by the US Army Aviation Test Board. These studies include:

- (1) Static Ground Evaluation where the pilot was observed by the evaluator following through flight envelope motions while stationary on the ground.
- (2) Flight Vibration Study where the retention of the armor insert was evaluated during the actual flight conditions.
- (3) Body Load and Pressure Evaluation to study the unseen loads and pressure exerted of the pilot's body by the survival/armor vest and the aircraft shoulder/lap belt restraint system.
- (4) A sizing study was conducted to develop criteria that could be used to expand the range of body sizes a vest would fit and reduce the number of no-fits.





#### DISCUSSION OF TESTS PERFORMED

#### 1. STATIC GROUND EVALUATION

#### A. OBJECTIVE:

To identify those areas contributing to the incompatibilities of the USAF Survival/Armor Vest with the pilot of an OH-58 Helicopter during his flight performance envelope.

#### B. METHOD OF EVALUATION:

The Survival/Armor Vest was worn by the pilot. The pilot that was chosen for these evaluations was selected at random. His body measurements are: Stature 62 in. (147.08 cm), chest circumference 44 in. (111.76 cm), and waist circumference 37 in. (93.98 cm). A large-regular size vest was issued to him for these evaluations. Only one pilot was chosen for this detailed follow-through on all evaluations of this OH-58 Helicopter. The pilot was observed by the evaluator and provided subjective reports that together formed the results of this evaluation. The front door of the OH-58 Helicopter was removed to facilitate photographing the pilot's actions. The pilot went through the following flight motions.

Releasing cyclic friction.
Reaching starter switch with right hand.
Reaching radio controls.
Adjusting restraint system.
Bringing cyclic to the rear.
Retrieving check list from floor.
Egressing from helicopter.

#### C. EQUIPMENT:

OH-58 Helicopter Serial Number 20632 USAF Survival Vest Concept US Army Flight Suit 16-mm Motion Picture Camera

#### D. EVALUATION RESULTS:

In releasing the cyclic friction, figures 3 & 4, the left top edge of the armor insert and carrier hit the pilot's chin. In bending forward and twisting to the right, the left bottom edge of the armor insert and carrier pressed into the waist area and the survival first aid kit pressed into the left leg. As the pilot reached for the starter switch and radio controls, figure 5, the armor insert and carrier restricted the right arm movement, rode up outside the chin; the shoulder harness then pressed into the neck, and the lap belt pressed the armor into the lags.

When the cyclic control was brought fully to the rear, the survival component, along with the right side edge of the armor insert, forced the right arm of the pilot outside the helicopter. During flight operations, the door is closed and the pilot is forced to use a wrist action or a twisting of the body to move the arm to go between the armor panel on the seat and his body.

The helicopter check list was on the floor of the fuselage and the pilot found it difficult to retrieve it. This check list is used for preflight check and landing check of instruments and controls. These problems were similar to those identified when he adjusted the Cyclic Friction in figure 3.

When egressing from the helicopter the pilot found himself restricted in the neck area and on the left leg, figure 6. The armor inscrt and carrier bottom edge dug into the left leg, figure 7, and restricted the leg from further movement in egress. The upward movement of the armor plate from the leg binds the chin when the head is bent forward to clear the top edge of the door exit, figure 8.

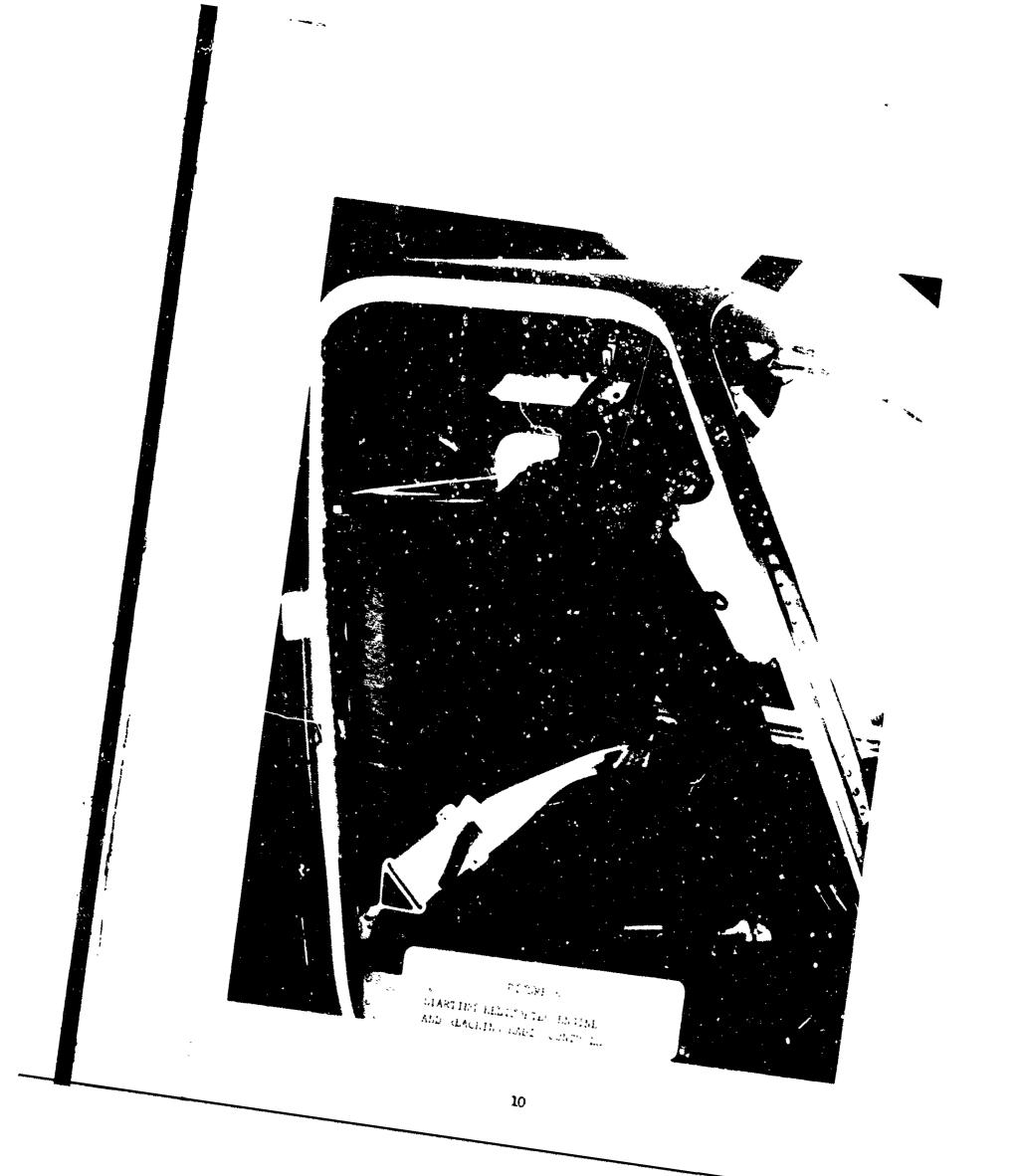
#### E. CONCLUSION:

The USAF Survival/Armor Vest with the armor insert will require redesign action to eliminate the binding caused by the armor insert on the arms, legs, and under the chin.

The aircraft cockpit design is limited. Its development did not consider the military pilot, his combat life support equipment, and the requirements of a military flight mission when designing the seats and pilot co-pilot mission envelopes.













#### 2. FLIGHT VIBRATION EVALUATION

#### A. OBJECTIVE:

To determine if the vest material and the design used in the fabrication of the vest can retain the armor carrier and insert in a safe position on the bodies of the pilot and co-pilot during helicopter flight. A safe position is considered to be one that does not restrict pilot or co-pilot motion or cause discomfort to the pilot or co-pilot during the flight operational envelope.

#### B. METHOD:

The Survival/Armor Vest was worn by the same pilot used in the static ground evaluation. The co-pilot flow the helicopter due to the flight safety hazards dited by the USA Aviation Test Board. (The pilot followed through on the controls.) The equipment was flown in the CH-58, since this helicopter was identified as having the worst human factor conditions cited in the US army Aviation Test Board Report (see page 2 ) that contributed to flight safety hazards. The flight was a mound robin type with normal routine flight precedures.

The vest was worn one inch off the legs of the pilot with the top edge of the carrier lined up with the upper edge of the breast bone. This position was checke for swement every ten minutes during flight. Due to the lack of control over the plate exament, flight was terminated after two hours.

#### C. TEST RESULTS:

The armor insert and carrier dropped an average of 3/8 in. to 5/8 in. every five minutes. At the end of ten minutes, the armor insert and earrier were resting on the legs with no where else to go. Every ten minutes, the armor insert and carrier were returned to the initial position and the pilot readjusted the shoulder harness and lap belt in an attempt to control the armor insert. The vest material and design did not provide adequate retention characteristics to keep the armor insert and carrier off the pilot's legs.

#### D. CONCLUSION:

The USAF Survival/Armor Vest requires redesigning of the vest to provide built-in support and retention for the armor insert to keep it up off the legs during flight operations.

## 3. BODY LOAD AND PRESSURE EVALUATION

#### A. OBJECTIVE:

To determine if the vest, armor insert, and carrier, when worn as a complete assembly, contribute to unseen load and pressure on the body of the pilot as he follows through on his flight envelope motion.

#### B. EQUIPMENT:

Oh-58 Helicopter at Ft. Devens, MA.
USAF Survival/Armor Vest
US Army Flight Suit
US Army NDC Load Profile Analyzer
16-mm Camera and Miscellaneous Equipment for recording evaluation.

#### EQUIPMENT NOTE:

The Load Profile Analyzer, figure 9, consists of four basic units: Load Sensing garment front and rear display consoles representing the upper torso, power supply, and remote control unit.

The load sensing garment is a front closure vest containing 248 pressure sensors. The sensors, figure 10, are arranged in a matrix similar to the display console and mounted on vertical strips of mylar tape. The tape is configures to follow the lines of the torso. Each tape is connected to the bottom to a wiring harness. The harness transmits the signal to the display units by means of an umbilical line.

Each pressure sensor on the garment is represented on the torso model by a tri-colored lamp which is energized by the sensor output. The yellow filament is energized to indicate that 0.5 lb of pressure is being placed on the sensor; the green filament indicates 1.0 lb and the red is 1.5 lb or more. The displays can be held in four action modes; accumulate, continuous, hold, and clear. In this evaluation the continuous mode was used to show continuity of a pilot's actions and their results on the display consoles.

A 16-mm Motion Picture Camera recorded the evaluation at 24 FPS. The results of this evaluation were arrived at through the use of a 16-mm Motion Picture Projector Analyzer and the stop action on the projector.

#### C. METHOD:

The sensor vest was worn under the USAF Survival/Armor Vest, the pilot then entered the helicopter in the pilot position. The umbilical line was connected between the sensor vest and the display console. The pilot proceeded to follow the same flight envelope motions that were used during the Statis Ground Evaluation. The pressure of the body load was transmitted to the display console. This information was recorded by 16-mm color film for future use by an analyzer projector.

#### D. TEST RESULTS:

Pressure loads developed in the right chest area when the pilot bent over to release the cyclic friction, figure 11, or reached over with his right hand to activate the starter switch and radio controls.

Right Chest pressure, figure 12, was caused by the shoulder harness which pressed down on the shoulder and the armor insert which pressed in on the body. As the pilot continued to bend forward, the lap belt buckle caused pressure on the waist and forced the armor insert and carrier into the lower abdomen.

In retrieving the helicopter flight check list from the floor, pressure was exerted on the abdomen. The top right edge of the armor insert was forced into the body  $r_f$  the right shoulder harness, figure 13.

Exiting the helicopter caused pressure on the center chest and just below the center of the rib cage, as shown in figure 4. The armor insert also exerted pressure in the waist as the pilot lifted his body to exit the helicopter.

#### E. CONCLUSION:

This evaluation details the loads on the body and affirms the problem areas found in the static ground evaluation. It also points to the sensitivity of the sensor vest and its possible value in substantiating a given problem on the body of an individual when wearing clothing and/or other equipment.

#### NOTE:

All test results are based on the number and location of 1-1/2-1b pressure loads imposed on the body as displayed on the console unit. Only the pressure loads on the front console unit were recorded for this evaluation.

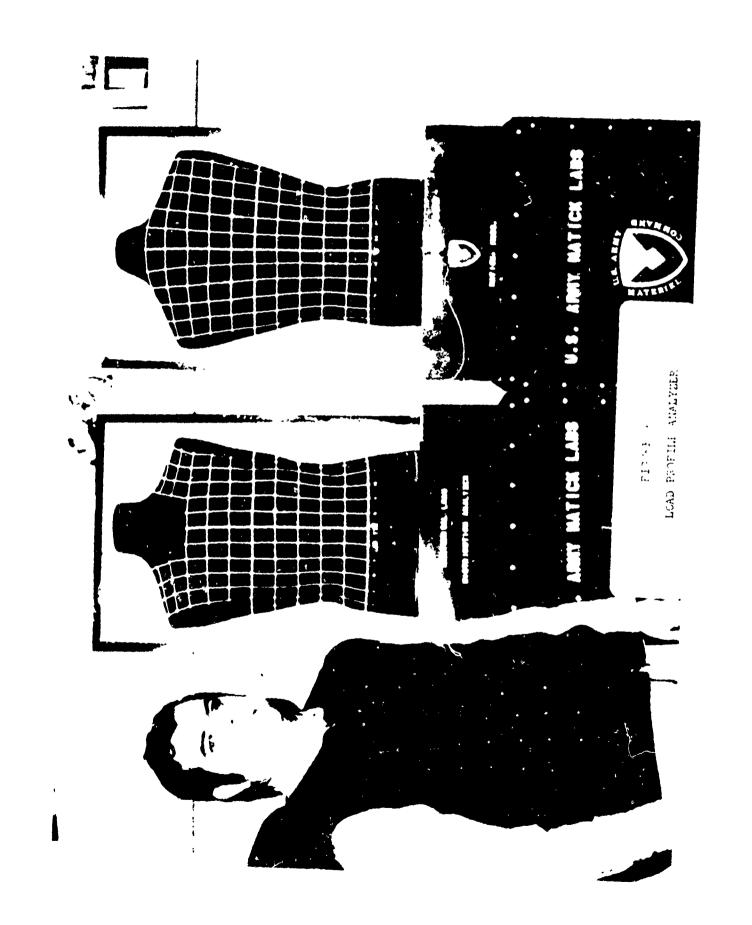






FIGURE 11
Reaching Cyclic Friction

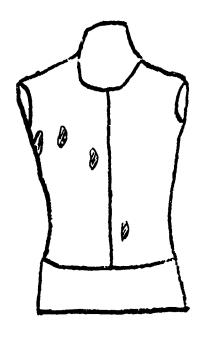


FIGURE 12
Bending Forward



FIGURE 13

Retrieving Helicopter Check List

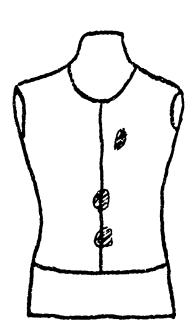


FIGURE 14

Exiting Helicopter

Load Profile Display Read Out

Areas of Pressure on the body 1 1/2 lbs and over

#### 4. SIZING CRITERIA EVALUATION

#### A. INTRODUCTION:

During the test program for the Individual Survival Vest for Aircremumbers at the USA Aviation Test Board, test subjects complained of poor fitting of both the USAF Survival/Armor Vest and the US Army Survival/Armor Vest and armor insert. Test Project Officers also felt that there was not enough flexibility in the present sizing criteria of both vest systems to adequately fit the aircrewman population. A study was initiated to evaluate the sizing criteria for the USAF and the US Army Armor insert at USA Natick Research and Development Command, since these items could be evaluated together, in order, using the same evaluation guidelines. Primary attention was placed on the armor insert—a non-flexible ceramic armor plate requiring a flexible sizing criterion, to enable these items to be used by a larger number of the aviation population.

#### B. OBJECTIVE:

To explore the possibility of expanding the present sizing criteria to cover a larger number of people in the aviation community.

#### C. EVALUATION METHODS AND RESULTS:

Bivariate charts will be used to illustrate and evolve the sizing systems. A bivariate chart is a cross tabulation of two variables presented in a table format. The first variable is along the Y axis and the second along the X axis. The sizing relationship of the two variables can then be blocked out on the charts.

Data from the 1966 US Army Anthropometric Survey and the 1970 US Army Aviators Anthropometry Survey were used to correlate fitting criteria. 3,4 The sample size of the anthropometric data base consisted of seventy body dimensions measured on 6682 individuals. The data were maintained in mass storage file on the Command's Univac 1106 computer facility. Software was developed to produce bivariate distributions of all relevant body dimensions. A data management file was constructed to test various sizing plans and optimize the fit.

The current sizing criteria for the two systems are based upon stature, chest circumference, and waist circumference (see Table 1). The bivariate representations of these systems are shown in Appendix A. An objective of the sizing system is to provide comfort and fit as well as proportionate area coverage for the individuals within a size range. The fit of the armor is primarily related to torso dimensions, and these dimensions should be the prime elements in obtaining the best fit. Correlation coefficients from

<sup>&</sup>lt;sup>3</sup>The Body Size of Soldiers US Army Anthropometric 1966, TR-72-51-CE, While R.M., NARADCOM, E. Churchill, Anthropology Research Project, Yellow Springs, OHIO, Dec. 1971.

Anthropometry of US Army Aviators 1970, Dec 1971, TR-72-52-CE, E. Churchill J.T. McConville, L.L. Lauback, Anthropology Research Project, Yellow Springs Ohio and R.M. White US Army MARADCOM, Matick, MA

the 1970 US Army Aviators Anthropometric Survey show that the correlations between stature and waist back and front length are poor, +0.560 and +0.427, respectively. These low correlations indicate that a more optimum sizing system could evolve through the use of a variable which correlates better with the torso dimensions. Such a variable is the standing vertical truck circumference which is measured by a steel tape passing through the crotch and over the midpoints of the right buttock and right shoulder. The correlations between standing vertical trunk circumference and waist back and front length are +0.630 and +0.700, respectively.

The actual surface dimensions of the front and back plates of the three-size body armor are shown in Table 2. These dimensions can be used as minimal fitting guidelines for a sizing system. Bivariate charts which relate these dimensions in terms of the waist back length, interscye breadth, and chest breadth are in Appendix B. The dimension which has the best correlation with waist back and front length is the vertical truck circumference. Bivariate representations of a three-size system utilizing vertical trunk, waist, and chest circumferences are shown in Appendix C. The sizing criteria using this system is shown in Table 3. Table 4 illustrates the fit statistics of both three-size systems. The vertical trunk sizing system as evidenced by Table 4, clearly involves a larger percentage of the population within the fitting scheme.

The same logic can be applied to the four-size aircrew armor system. The actual surface dimensions of the front and back plates of the four-size system are shown in Table 5. The four-size system is different from the three-size in that the difference between the regular and the long size is in the plate length. This arrangement allows for a blocking type of sizing system which does not overlap. Bivariate representations of the current and proposed sizing systems are shown in Appendix D and E. Table 6 shows a comparison of the fit statistics for both four-size systems. This table illustrates the large involvement of individuals within the fitting scheme when the vertical trunk circumference is used as a criterion. Table 7 represents the four-size system incorporating the standing vertical trunk circumference.

#### D. CONCLUSION:

It is evident that using the vertical trunk circumference as a sizing variable will result in a large involvement of individuals in the fitting scheme.

TABLE 1

# Current Sizing Criteria for Air Crew Armor Insert

# US Army Three-Size System

| Silly TT            | _             |
|---------------------|---------------|
| Stature             | thru 67.0 in. |
| Chest Circumference | thru 37.5 in. |

Waist Circumference thru 32.0 in.

# Regular

| Stature             | 67.0 in. thru 70.5 in. |
|---------------------|------------------------|
| Chest Circumference | 37.5 in. thru 41.5 in. |
| Waist Circumference | 32.0 in. thru 40.0 in. |

# Long

| Stature             | greater than 70.5 in. |
|---------------------|-----------------------|
| Chest Circumference | greater than 41.5 in. |
| Waist Circumference | greater than 36.0 in. |

# USAF Four-Size System

| Medium Regular      |                        |
|---------------------|------------------------|
| Stature             | 63.0 in. thru 67.0 in. |
| Chest Circumference | 29.5 in. thru 37.0 in. |
| Waist Circumference | 28.0 in. thru 32.0 in. |

## Medium Long

| Stature             | 67.0 | in. | thru | 73.0 | in. |
|---------------------|------|-----|------|------|-----|
| Chest Circumference | 37.0 | in. | thru | 43.5 | in. |
| Waist Circumference | 32.0 | in. | thru | 40.0 | in. |

## Large Regular

| Stature             | 55•5 | in. | thru | 72.0 | in. |
|---------------------|------|-----|------|------|-----|
| Chest Circumference | 35.5 | in. | thru | 42.0 | in. |
| Waist Circumference | 36.5 | in. | thru | 38.5 | in. |

# Large Long

| Stature /           | 70.5 in. thru 75.0 in. |
|---------------------|------------------------|
| Chest Circumference | 40.5 in. thru 45.5 in. |
| Waist Circumference | 36.5 in. thru 43.0 in. |

TABLE 2
Surface Dimension of Front and Back Plate
US Army Aircrewman Body Armor

## Pimensions in Inches

# Three Size System

|         | Waist<br>Back<br>Length | Waist<br>Front<br>Length | Chest<br>Breadth | Interscye<br>Breadth | Waist<br>Circumference | Chest<br>Circumference |
|---------|-------------------------|--------------------------|------------------|----------------------|------------------------|------------------------|
| Long    | 18.6                    | 16.10                    | 11.17            | 14.25                | 35.8                   | 25.4                   |
| Regular | 16.6                    | 15.00                    | 9.62             | 13.00                | 31.2                   | 22.6                   |
| Short   | 14.7                    | 13.85                    | 9.62             | 11.25                | 28.7                   | 20.9                   |
|         |                         |                          |                  |                      |                        |                        |

TABLE 3

# Proposed Sizing System for Air Crew Armor Statistics Based on 1966 US Army Data

### Unit of Measure is Inches

# Three Size System

| Measure                         | Moun | Std. Dev | Minimum | Maximum       |
|---------------------------------|------|----------|---------|---------------|
| Vertical Trunk<br>Circumference | 64.6 | 3.3      | 53.3    | 78.2          |
| Chest Circumference             | 36.9 | 2.62     | 28.35   | 48.89         |
| Waist Circumference             | 31.6 | 3.24     | 23.14   | 50 <b>.27</b> |

# Sizing Criteria

| Small   |          |      | Vertical Trunk Circumference | LF | 64.0 | in. |
|---------|----------|------|------------------------------|----|------|-----|
|         |          |      | Chest Circumference          | LE | 37.5 | in. |
|         |          |      | Waist Circumference          | LE | 30.0 | in. |
| Regular | 64.0 in. | .LT. | Vertical Trunk Circumference | LΞ | 68.0 | in. |
| -       | 35.5 in. | .LT. | Chest Circumference          | LE | 41.5 | in. |
|         | 30.0 in. | .LT. | Waist Circumference          | LE | 36.0 | in. |
| Long    |          |      | Vertical Trunk Circumference | GT | 68.0 | in. |
| J       |          |      | Chest Circumference          | GT | 39.5 | in. |
|         |          |      | Waist Circumference          | GT | 36.0 | in. |

TABLE 4

# Air Crew Armor Fit Statistics

Total In Survey 6681

# Fit Using Stature, Waist & Chest Circumference

| No. Short   | 1081 | 16.18 % |
|-------------|------|---------|
| No. Regular | 564  | 8.44 %  |
| No. Long    | 63   | •94 %   |
| No. No Fits | 4973 | 74.43 % |

# Fit Using Vertical Trunk, Waist & Chest Circumference

| No. Short   | 1580 | 23.65 % |
|-------------|------|---------|
| No. Regular | 1621 | 24.26 % |
| No. Long    | 359  | 5.37 %  |
| No. No Fits | 3121 | 46.71 % |

TABLE 5
Dimensions of Four-Size USAF Air Crew Armor Plates\*

|                | Front Plate |         |         | Back Plates |         |         |
|----------------|-------------|---------|---------|-------------|---------|---------|
|                | Weist       | Chest   | Waist   | Waist       | Chest   | Waist   |
|                | Front       | Breadth | Breadth | Back        | Breadth | Breadth |
| Medium Regular | 13 1/16     | 8 5/8   | 12 3/4  | 15 3/8      | 9 1/2   | 12 1/2  |
| Medium Long    | 14 9/16     | 8 5/8   | 12 3/4  | 16 3/8      | 9 5/8   | 12 1/2  |
| Large Regular  | 14 1/16     | 10 1/16 | 15 1/2  | 15 1/2      | 10 7/16 | 14 7/8  |
| Large Long     | 15 9/16     | 9 15/16 | 15 1/2  | 17          | 10 1/8  | 14 3/4  |

<sup>\*</sup> All dimensions ± 1/8 inch

TABLE 6

# Air Crew Armor Fit Statistics

# Four Siga System

Total in Survey 6681

# Fit Using Stature, Waist & Chest Circumferences

| Medium Regular | 694  | 10.39 % |
|----------------|------|---------|
| Medium Long    | 1370 | 20.51 % |
| Large Regular  | 176  | 2.63 %  |
| Large Long     | 118  | 1.77 %  |
| No Fits        | 4323 | 64.71 % |

# Fit Using Vertical Trunk, Waist & Chest Circumferences

| Medium Regular | 2234 | 33.44 % |
|----------------|------|---------|
| Medium Long    | 1228 | 18.3    |
| Large Reguler  | 610  | 9.13 %  |
| Large Long     | 1124 | 16.82 % |
| No Fits        | 1485 | 22.23 % |

TABLE 7

#### Proposed USAF Aircrew Armor Insert Four Size System

# Medium Regular

| Chest Circumference          | 31 | inches | thru | 37. | 5 inches |
|------------------------------|----|--------|------|-----|----------|
| Waist Circumference          | 26 | inches | thru | 32  | inches   |
| Vertical Trunk Circumference | 57 | inches | thru | 64  | inches   |

### Medium Long

| Chest Circumference          | 31 | inches | thru | 37.5 inches |
|------------------------------|----|--------|------|-------------|
| Waist Circumference          | 26 | inches | thru | 32 inches   |
| Vertical Trunk Circumference | 64 | inches | thru | 68 inches   |

### Large Regular

| Chest Circumference          | 37.5 inches thru 42.5 inches |
|------------------------------|------------------------------|
| Waist Circumference          | 32.0 inches thru 40.0 inches |
| Vertical Trunk Circumference | 59.0 inches thru 66.0 inches |

## Large Long

| Chest Circumference          | 37.5 inches thru 44.5 inches |
|------------------------------|------------------------------|
| Waist Circumference          | 32 inches thru 41 inches     |
| Vertical Trunk Circumference | 66 inches thru 74 inches     |

#### CONSOLIDATED RECOMMENDATIONS

1. STATIC GROUND EVALUATION AND BODY LOAD AND PRESSURE EVALUATION: A dimensional profile study should be conducted to determine suitable height, length, and width measurements that would eliminate the binding on the pilot's body.

Modify the armor carrier to meet those dimensional recommednations developed during the proposal profile study.

2. FLIGHT VIBRATION EVALUATION: Redesign the vest as follows: study the replacement of the reschel knit nomex material as a basic support material; build in a harness under the basic vest material to add strength to support the weight of the armor carrier and insert to restrain its movement. Improve the design by using lighter weight materials for armor carrier construction.

warnings should be issued to all pilots not to use the survival components pockets under the right arm when flying the OH-58 type helicopter.

3. SIZING EVALUATION: Conduct a human factors evaluation to determine if the proposed computer sizing criteria can be utilized as a practical substitution for the present sizing criteria now used by the USAF Survival/Armor Vest.

Appendix A
Bivariate Representations of Current Sizing Systems

STATURE (IN) VS CHEST CIP-UNFERENCE (IN)

| 8        | 25.50      | 27.50  | 29.50      | 20       | 31.50 | 33.50  | 35,50      |       | 37.50  | 39.50    | 41.50 |      | 43.50 | 45.50      | •       |
|----------|------------|--------|------------|----------|-------|--------|------------|-------|--------|----------|-------|------|-------|------------|---------|
|          |            | • 00•  | ٠<br>8     | 00.      | • .00 | •      | ÷          | * *** | .00    | ·<br>•   |       | 8.   | 8     | ฮ.<br>• .  | .35     |
| + 3      | •          | 8.     | 8          | 8.       |       | . 00.  | 8.         | ю.    | 8.     | ð.       |       | ន    | ਰ.    | 8.         | .16     |
| + 8 8    | •          | . 00.  | 8          | 3.       |       | . 00.  | 9.         | 60.   | ₹.     | .07      |       | ŧ.   | 8.    | 00.        | .s.     |
| + 00.57  | •          | . 00.  | 00.        | 8        |       | . 8.   | 60°        | .33   | .52    | .27      |       | ಕ್ಕ  | ē.    | <b>8</b> . | 1.32    |
|          | ٠          | , 00.  | 00.        | 8.       | .00   |        | <b>š</b> . | .73   | .81    | .57      | Ne    | .19  | ē.    | a.         | 2.8     |
| 3 5      | •          | . 00.  | 8          | 8        |       | .15    | š.         | 1.68  | 1.24   | 1.03     |       | .38  | .15   | 60.        | 5.57    |
| + 75.57  | ~ <b>,</b> | . 00.  | 00.        | 8.       |       | .25 1. | 1.35       | 2.87  | 2.13   | <b>₹</b> |       | 94.  | 8     | 6.         | 8.14    |
| • •      | •          | ٠٠ ٥٥٠ | 00.        | .00      | £4.   |        | 2,33       | 3.74  | 2.59   | 1.38     |       | .37  | ¥.    | 60.        | 11.18   |
| + 00.07  | •          | . 00.  | 8.         | ē.       |       | .69 2. | 2.84       | 46.4  | 7 3.40 | 1.65     |       | 8.   | .15   | 3 .12      | 14.41   |
| • 65.60  | •          | . 00.  | 8.         | 8.       | 1.15  |        | 3.91       | 5.21  | 3.32   | 1.18     |       | • 55 | .16   | 60.        | 15.61   |
| • 6      | <u>,</u>   | . 00.  | 00.        | .10      | 1.09  |        | 60.4       | 4.82  | ₹2.75  | 1.23     |       | 30   | .10   | 8.         | 14.52   |
| 3.6      | •          | 00.    | 6          | 01.      | 76.   |        | 3.23       | 3.5   | 2.24   | 3.       | t     | *24  | .10   | 90.        | ž.<br>1 |
|          | •          | . 00.  | 8.         | .00      | 37.   |        | 2.02       | 2.08  | 1.26   | .61      |       | .12  | 90.   | 900        | 7.00    |
|          | •          | . 00.  | <b>a</b> . | 90.      | 15.   |        | 1.17       | 1.11  | 3.     | .15      |       | .00  | 8.    | 00         | 3.0     |
| <u> </u> | -•         | . 00.  | 8.         | .0       | .31   |        | .52        | 8 n.  | .36    | .19      | _     | 90•  | ਰ     |            | 2.02    |
| Ī        | -•         | . 00.  | 8.         | .00      |       | . 22   | .30        | .19   | .15    | 00.      |       | %    | .00   | 00.        | .87     |
| 3        | •          | . 00.  | 8.         | <b>š</b> | .15   |        | .10        | 60.   | .00    | .01      |       | 8.   | 8.    | 8.         | 87.     |
|          | -•         | . 00.  | 8.         | ъ.       | . 03  |        | 36.        | 10.   | %      | 00.      |       | .01  | 00.   | a.         | .15     |
|          |            | %      | 10.        | .55      | 6.82  |        | 23.60      | 32.07 | 21.73  | 8.6      |       | 3.38 | 1.23  | 19.        | 100.00  |

1966 - U. C. APPY ANTHROPORETRY SURVEY STATURE (IN) VS WAIST CIRCUMFERENCE (IN) CUPPERT THREE-SIZE SYSTEM

|             | <b>26.</b> 00 | 28.00 |       | 30.00   | 32.00           | 34,03      | 35.00           | 00 | 38.00     | 0°.0° | 42.00      | 00.44    | <b>*6.0</b> C | •          |         |
|-------------|---------------|-------|-------|---------|-----------------|------------|-----------------|----|-----------|-------|------------|----------|---------------|------------|---------|
|             |               | 00.   | ಕ.    | ~.      | 8               | æ.         | <b>60</b> .     | •  | 00.       | 8.    |            | . 30     | ส.            | 8          | .15     |
| 77.00.4     |               | 8.    | 8.    | ٠.      | ន               | 8.         | 3.              | •  | . u.      | 00.   |            | 00.      | G.            | 8          | .16     |
| * 00.4      |               | 8.    | ь.    | •       | 1 è             | .10        | ة<br><u>5</u> ( |    | .00       | 8.    | æ.         | 8        | <u>ي</u> .    | 8          | .57     |
| + 98°52     |               | 8.    | .15   | • •     | .33             | .28        | S.              |    | .13 .04   | 60*   | 10.        | 4        | (3.           | <b>ة</b>   | 1.32    |
| ÷ 95. %     |               | .10   | 3     | ~       | 69              | 09.        | 64.             | o  | 81. 81.   | 60*   | 00.        | Q        | .23           | 8          | 2.88    |
| + 8.57      |               | .16   | 56.   | 1.59    | 65              | 1.15       | .73             | 1  | .49 .21   | .10   |            | ٠<br>. : | 8.            | 8          | 5.57    |
| + 02.27     |               | .51   | 1.59  | 2.42    | 24              | 1,78       | .87             | •  | . 33      | \$1.  | <b>5</b> . |          | 8.            | 8          | *       |
| • 90.47     |               | 6 *   | 2.53  | 2.0     | 8               | 2.50       | 1.48            |    | ¥6. 49.   | .12   | g.         | 9        | 96.           | 8          | 11.18   |
| • 6         |               |       | 3.46  | 4.10    |                 | 2,65       | 1.60            | 7. | 1.03 .40  | .15   | •10        | 0        | 8.            | <b>a</b> . | 14.41   |
| ÷ 66.       | •             | 1,30  | K.22  | 3       | ة<br><u>0 ك</u> | 2.48       | 1.32            | •  | .82 .45   | .18   | .00        | •        | ນລ•           | ន          | 15,61   |
| 8 9         | -             | 1.65  | 3.95  | *       | <u>52.</u><br>: | 2.35       | 1,35            | •  | .42 .16   | .12   | 5.         |          | · 30          | 8          | 14.52   |
| 80.79       |               | 1.63  | 3.29  | 2.95    | 38              | 1.74       | .91             |    | 31. 75.   | 32    | 8.         | 9        | 63.           | 8          | и.<br>В |
| • 6         | •             | 3.8   | 2.32  | 7       | - 65            | š.         | .51             | •  | .39       | .00   | ន          | 9        | 60.           | 8          | 1.00    |
| 1           |               | .72   | 1.14  | <b></b> | 88              | 6<br>*     | .21             | •  | .15 .01   | 8.    |            | 00.      | 00.           | 8          | 3.64    |
| 3<br>3<br>3 |               | 64.   | .57   | •       | 37              | .24        | .27             | •  | w. w.     | 8     |            | .00      | .00           | 8          | 2.02    |
| O 1         |               | .33   | .21   |         | 19              | .10        | .03             | •  | .00       | 8.    |            | 00.      | · 00          | 8          | .87     |
| 4 5         |               | .19   | .12   | •       | 60              | <b>š</b> . | ق               | •  | 00.       | 00.   |            | .00      | .00           | 8          | æ<br>*. |
|             |               | ۶.    | 8     | -       | 8               | .01        | %               | •  | .01       | 00.   | 10.        | <b>4</b> | 00.           | 8          | .15     |
|             | 1             |       |       |         | 1               |            | 9               | 1  | Ì         |       |            | 5.5      | .15           | 8          | 100.00  |
|             |               | 25.   | 25.28 | 27.(    | 61              | 17.57      | 10.18           | ň  | 5.27 2.48 | 1.27  |            | 2        | 3             |            | ,       |

1966 - U. S. ARMY ANTHROPOMETRY SURVEY HAIST CIRCURFERENCE (IN) VS CHEST CINCUNFERENCE (IN) CURRENT THREE-SIZE SYSTEM

|            |             |            |       |              |       | ,        | 1     | THE PROPERTY OF | CONTRACT SINCE SISSES |          |       |      |     |       |       |     |        |
|------------|-------------|------------|-------|--------------|-------|----------|-------|-----------------|-----------------------|----------|-------|------|-----|-------|-------|-----|--------|
| Α,         | <b>3.</b> 6 | 30.00      | •     | 32.00        | 34.00 | ₩<br>₩   | 35.00 | 38.00           | 00.00                 | _        | 42.00 | 00 + | a a | 46.00 | 48.00 | •   |        |
| ,          |             | 24.        | 8.    |              | 8.    | <u>9</u> | 5     | 00.             | .01                   | .00      | ٠     | 96.  | ಕ   | •     | ន     | ۵.  | 81.    |
| * 35.7     |             | 06.        | 8     |              | 00.   | 70.      | ~     | 8.              | ē.                    | 60.      | •     | .15  | 8   | •     | 8.    | 9.  | 2      |
| • 00.5     |             | 90.        | .00   |              | 8.    | 07.      | 77    | .22             | .31                   | .37      | •     | .13  | ಕ್ಕ | •     | 00.   | 8   | 1.23   |
| • 06.7     |             | <b>a</b> . | a     |              | .13   | 79,      |       | 1.14            | .81                   | 9.       | •     | .13  | ē.  | •     | .02   | 8   | 3.38   |
|            |             | .16        | .81   | 1            | 2.32  | 3.02     |       | 2.39            | <b>3</b> .            | .30      |       | 8.   | 8   |       | 00.   | 8   | 86.6   |
| + 00 h     | # <b>i</b>  | 1,80 6,    | 6,18  | 38           | 7.42  | 4.79     | •     | 1.29            | .24                   | 8.       | •     | .01  | 00. | •     | .00   | 00. | 21.73  |
| 27.50      |             | 9.50 14    | 14.25 | L            | 6.54  | 1.47     |       | .10             | .30                   | 8.       | •     | 00.  | 8.  | •     | • 00  | 00. | 32.07  |
|            | 16          | 16.61 5.   | 5.87  | <del>,</del> | 8     | .15      |       | 8.              | 70.                   | 00.      | •     | 00.  | 00. | •     | 00.   | 00. | 23.60  |
|            | 49          | 6.21       | 8     |              | .09   | ٥.       |       | 8.              | 00.                   | 8        | •     | .00  | 00. | •     | 00.   | 8.  | 6.82   |
|            |             | 5          | 8     |              | 00.   | 9.       |       | 00.             | 00.                   | <b>.</b> | •     | .00  | 00. | •     | 00.   | 00. | .55    |
| 1 9        |             | <b>a</b> . | 8     | ···-         | 00.   | 8        |       | 80.             | 00.                   | 00.      | •     | . 60 | 00. | •     | 00.   | 00. | ਰ.     |
| 25.50 + 0. | -           | 90.        | 8.    |              | 69    | 9.       |       | 00              | 8                     | 00.      | •     | • 00 | 8   | •     | 00.   | 90. | 00.    |
|            | Ä           | 34.85 27   | 77.61 | 15           | 17.57 | 10.18    |       | 5.27            | 2.48                  | 1.27     |       | .52  | .15 |       | .07   | 10. | 100.00 |

1366 - U. S. ARMY ANTHROPOPETRY SURVEY CHEST CIRCUPFLMENCE VS WAIST CIRCUMFERENCE CURPENT FOUR-SIZE SYTTEM

|         |     |     |               |      |      |           | ,               |      |      | ,        | 1    |      |      | •        | •    | •    |    |      |
|---------|-----|-----|---------------|------|------|-----------|-----------------|------|------|----------|------|------|------|----------|------|------|----|------|
| 26.0    | 9.0 | e.  | 2 <b>9.</b> 0 | 30.0 | 31.0 | 32.0      | ນ <b>.</b><br>ຄ | 0.46 | 35.0 | 36.0     | 37.0 | 38.0 | 0.65 | C •      | 0.14 | *2.0 | •  |      |
| •       | •   | 0,  | •             | 0.   | •    | ,<br>o    | •               | •    |      | 0.       | •    |      | . 0. | T.       |      | ٦.   | •  | 6.   |
| + 05. 3 | o.  | o.  | e.            | o.   | o.   | o.        | •               | •    | •    | ٦:       | •    | ٦.   | 7.   | 7        | 7.   | ۲.   | 7. | 1.0  |
| + 05.50 | •   | ٥.  | °.            | ٥.   | 0.   | ٠,        | ۰.              | o.   | 7    | ١.       | 7.   | ٠.   | -    | .2       | •5   | ۲.   | 7  | 1.3  |
| + 05.54 | o.  | ۰.  | o.            | ٥.   | o.   | ۰.        | ٥.              | ۲.   | .2   | r.       | 3.   | ۳.   | ~~   | ~        | 7.   | 7    | 7  | 2.1  |
| DC . T  | o.  | á   | o,            | •    | 7    | ٦:        | .2              | ۳.   | 3.   | ۲.       | ٠٤   | ٠.   | ₃.   | .2       | ٦٠   | .1   | 0. | 4.0  |
| + 05.04 | °.  | 0   | ຕຸ            | 7    | 7.   | ₹.        |                 | 1.0  | 1.0  | σ.       |      | s.   | .2   | 1.       | 0.   | o,   | ٥. | 6.0  |
| + pc.85 | •   | °.  | 7             | ₹.   | ۲.   | F. 1      | 1.8             | 1.7  | 1.5  |          | ٠    | ۳.   | -:   | -:       | ٥.   | 6.   | ۰, | 9.7  |
| ÷ 5     | e.  | 7.  | ۲.            | 1.0  | 1.8  | 2.3       | 2.3             | 1.5  | 1.5  | ٠.       | r.   | 7.   | 7.   | ۰.       | o.   | c.   | 0  | 12.1 |
| 00.16   | 7,  | .2  | 6.            | 2.0  | 2.8  | 3.5       | 2.6             | 1.6  | 8.   | -<br> -: |      | o.   | °.   | o.       | ٥.   | ٥.   | ó  | 14.8 |
| + 00.00 | 7   | ۲.  | 1.7           | 3.9  | 4.2  | 3.7       | 1.8             | ۲۰   | ۴,   | ٦.       | •    | ٥.   | o,   | o.       | ٥.   | ပ္   | ٥. | 17.2 |
| 4 00.00 | ۳.  | 1.5 | 2,7           | 0.   | 2.9  | 1.6       | ø.              | ٠.   | ۲.   | ę.       | e.   | o.   | o.   | ۰.       | e,   | ပ္   | •  | 9.51 |
| + 05'45 | ø.  | 9.7 | 3~2           | 2.6  | 1.0  | <b></b> - | 7.              | ٥.   | o.   | o.       | o.   | e.   | ٥.   | <b>ٿ</b> | e.   | ٥.   | ٥. | 9.7  |
| + no or | ð,  | 1.0 | 1.1           | æ    | ຕຸ   | ٦.        | 7.              | ສຸ   | 0,   | •        | o.   | 0.   | ٥.   | ٥.       | ٥.   | o.   | o. | 5.1  |
| 32.50   | e.  | æ.  |               | ۲.   | 7    | o,        | 0               | o,   | ٥.   | ပ္       | o.   | 0.   | ó    | o.       | •    | o,   | ç. | 2.3  |
| }       |     |     |               |      |      |           |                 |      |      |          |      |      |      |          |      |      |    |      |
|         |     |     |               |      |      |           |                 |      |      |          |      |      |      |          |      |      |    |      |

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1966 - U.S. ARMY ANTHROPOMETRY STRUCE STATUPE (INCHES) VS CHEST CINCUMFERENCE CUPRENT FOUP-SIZE SYSTEM

The second of th

| 31.5  | 2.5<br>4.5<br>4.5<br>4.5<br>4.5<br>4.5<br>4.5<br>4.5<br>4.5<br>4.5<br>4 | ٠.<br>د د د د د د د د د د د د د د د د د د د | ٠.<br>د. | 7.05     |     | •    | 0.00 | 0.40       | n • |     | 5.7 | ?<br>? | •      | •  |      |
|-------|---|---|----------|----------|-----|------|------|------------|-----|-----|-----|--------|--------|----|------|
|       | •   | •   |          | o,       | •   | · -: | . 2. | . 2.       | •   | 7   | •   |        | ·<br>: | •  | 6.   |
| 93.67 | •   | •   | •        | o.       | ۲.  | .2   | е,   | ۴.         | 믁   | 7.  | ۰.  | •      | •      | •  | 1.3  |
| 3 5   | ė.  | e.  | .2       | .3       | e.  | *.   | 7,   | <b>3</b> . | .3  | .3  | ٦.  | ٠,     | •      | •  | 3.0  |
|       | ó   | ٦,  | ą,       | ٠        | ø.  | æ    | ۲.   | 9.         | 9.  | *.  | .2  | .1     | 7      | 7. | 5.6  |
|       | o.  | 7   | 'n       | <u>.</u> | 1.6 | 1.3  | 1.2  | o.         | 9.  | ь.  | F:  | 7.     | °.     | 7  | 8.1  |
|       | 7   | *.  | 1.0      | 7.       | 1.8 | 6:1  | 1.5  | 1:1        | œ.  | 9.  | .2  | .::    | .2     | 7  | 11.2 |
| , ,   | 7.  | νį  | 1.0      | 1.8      | 2.5 | 2.4  | 1.8  | 1.6        | 1.1 | · . | E,  | F:     | 7:     | 77 | 1    |
| 3 6   | 6.  | e,  | 3.4      | 2.5      | 2.8 | 2.4  | 1.9  | ŋ. E       | ø.  | 9.  | ۴.  | 7      | 7      | 7  | 15.6 |
| 3 8   | ۳.  | 6.  | 3.6      | 2.5      | 2.9 | 1.9  | 1.5  | 1.3        | ٠.  | s.  | .2  | ٠,     | 7.     | ۰. | 34.5 |
|       | s.  | 9.  | 1.3      | 1.9      | 2.1 | 1.6  | 1.1  | 1.1        | s.  | .2  | 7:  | ٠1.    | 7.     | 7  | n.2  |
| 3 8   | e.  | 'n  | 1.1      | 6.       | 1.2 | 6.   | 8.   | ₹.         | е.  | m,  | ۳:  | ٥.     | •      | •  | 7.0  |
| 3 6   | ~   | •   | 9.       | å        | 9.  | 5.   | 6.   | .2         | ۲.  | 7:  | 0.  | ٥.     | 0,     | o. | 3.6  |
| 3 8   | ۲.  | 7.  | ۴.       | .2.      | e.  | .2   | 2.   | ۲:         | 7   | ٥.  | ٥.  | ć.     | ۰.     | °. | 2.0  |
| 3     | .2  | E,  | .2       | £,       | ۲.  | 7-,  | ٠:   | 7.         | •   | •   | °.  | ٥.     | ۰.     | ٥. | 1.5  |

100.0

6.

1.0

1,3

2.1

0.4

6.0

4.1

12.1

14.8

17.2

13.9

9.7

5.1

2,3

1956 - J. S. APMY ANTHROPOMETRY SURVEY STATUPE (INCHES) VS MAIST CIRCUMPERENCE CUPRENT FOUR-SIZE SYSTEM

| 28.0       29.0       31.0       32.0       33.7       34.3         .0       .0       .1       .1       .1       .0       .1         .0       .0       .1       .2       .2       .2       .1       .1         .1       .2       .2       .2       .2       .1       .1       .0       .1         .1       .3       .7       .7       .7       .9       .6       .5       .8         .4       1.0       1.1       1.3       1.0       .8       1.0       .8       .9       .8       .8       .9       .8       .9       .8       .9       .9       .9       .9       .9       .8       .9 |
|--|
| 0 25.0 30.0<br>.0 .1 .1 .2 .4 .1 .1 .2 .2 .4 .2 .2 .2 .2 .2 .2 .2 .2 .2 .2 .2 .2 .2  |
|  |
|  |

.8 100.0

s.

Φ,

1.1

2.4

2.9

4,2

5.9

, ,

10.2

13.6

14.0

14.9

10.4

6.7

Appendix B
Bivariates of Torso Dimensions as Related to Fit

1966 - U. S. ARMY ANTHROPOMETRY SURVEY "A IST BACK LENGTH VS INTERSCYE

| 13.00    |          | 13.50 | 14.00      | 14.50 | 15.00  |         | 15.50 | 16.00 | 16.50    | 17.00  | 17.50 | 18.00 |            |            |
|----------|----------|-------|------------|-------|--------|---------|-------|-------|----------|--------|-------|-------|------------|------------|
| <b>*</b> | •<br>8   | 8     | •<br>•     | +     | •<br>8 | •<br>8. | 8.    | .01   | <b>+</b> | . 69.  | 8.    | .01   | 8          | .16        |
|          | <b>ਰ</b> | 6.    | 8          | £     | 90.    | .12     | .12   | 8.    |          | 90•    | 90.   | .01   | <b>E</b> . | 3.         |
|          | .12      | .21   | 7.         | .19   | 94.    | .67     | 8.    | .42   |          | .61    | .45   | .18   | .18        | <b>60.</b> |
|          | <b>š</b> | 3     | •          | . 90  | 1.41   | 1.72    | 2.20  | 1.78  | ~        | 1.62   | .87   | .57   | .51        | 12.84      |
| 7        | 1.32     | 1,56  | 2.38       |       | 3.17   | 3.55    | 60.4  | 3.19  | 14       | 2.05 1 | 1.48  | • 60  | 04.        | 23.78      |
| 4        | 3.1      | 1.63  | 2,83       |       | 4.27   | 4.50    | *     | 3.28  | 14       | 2.02   | 1.50  | .76   | .51        | 77.19      |
| <b>ત</b> | 1.74     | 1.57  | 2.56       |       | 3.29   | 3,83    | 3.37  | 2.47  | 7        | 1.30   | .91   | •24   | Ŗ.         | 23.52      |
|          | .73      | .70   | 1.32       |       | 1.45   | 1.42    | 1.11  | .73   |          | S #•   | .19   | 90.   | <b>a</b> . | 8.19       |
|          | r.       | .15   | 7          | .10   | •22    | .30     | .18   | 60°   |          | 8.     | 8.    | š.    | 00.        | 1.51       |
|          | 8.       | 8.    | <b>a</b> . | #     | 9.     | 8       | 00.   | 6.    |          | 00.    | 8.    | 00.   | 8          |            |
| 1 °      | 6.50     | 6.47  | 10.45      |       | 14.38  | 16.12   | 18.91 | 12.05 | "        | 8.20 5 | 5, 52 | 2.48  | 1.83       | 100.00     |

1966 - U. S. ARMY ANTHROPOMETRY SURVEY MAIST BACK LENGTH VS CHEST BREADTH

- でいからのこのなどのないのではないできるのではないのできるのです。

| 10.00 |            | 8.1<br>1.8 | 11.50      | 12,00 | 12.50 | 13.00      | 13.50      | ]4°00             | 14.50<br>+ | 15.00 |            | 4 |
|-------|------------|------------|------------|-------|-------|------------|------------|-------------------|------------|-------|------------|---|
| •     | 8          | 8.         | ਰ.         | ಕ್ಕ   |       | .00        | .00        | , <sub>70</sub> . | 00°        | . 00• | <b>a</b> . | • |
|       | œ.         | 8.         | <b>8</b> . | .15   | .16   | 60.        | .00        | 90•               | 00.        | .01   | ន          |   |
|       | <b>ð</b> . | £1.        | .37        | .75   | 1.03  | .79        | 87.        | .30               | .16        | ₹.    | 8          |   |
|       | .10        | .75        | 1.63       | 2,63  | 3.34  | 2.10       | 1.11       | .61               | .36        | •10   | .10        |   |
|       |            | 1.47       |            | 4.92  | 5.96  | 3,89       | 1.64       | .87               | .36        | .10   | ន          |   |
|       |            |            |            | 6.27  | 5.94  | 4,31       | 1,86       | .67               | .33        | .00   | ಕ          |   |
|       | 09.        |            |            | 5.40  | 4.67  | 2.74       | 1.08       | . # S             | .21        | ₹.    | a.         |   |
|       | .36        | .60        |            | 2,33  | 1.54  | 06.        | ъ <b>.</b> | .10               | .01        | 00.   | 8.         |   |
|       | 87.        |            | £4.        | .28   | .31   | <b>3</b> . | ສ.         | 00.               | 00.        | 00.   | 00.        |   |
|       | 8.         | <b>a</b> . | 00.        | 00.   | ю.    | .01        | 00.        | %                 | 00.        | 00.   | 00.        |   |

.25 100,00

•39

7.44

3.11

6.81

14.89

23.00

22.79

17.18

7.8

2,16

1966 - U. S. ARNY ANTHROPONETRY SURVEY VERTICAL TRUNK CINCUMFERENCE VS INTERSCYE

| c       |       |            |            |            |       |            |            |            |       |       |       |            |       |               |             |       |
|---------|-------|------------|------------|------------|-------|------------|------------|------------|-------|-------|-------|------------|-------|---------------|-------------|-------|
| •       | 13.00 | 13.50      | ā T        | 24.00<br>+ | 14.50 | 15.00      |            | 15.50      | 16.00 | 16,50 | 17.00 |            | 17.50 | <b>18.</b> 00 | •           |       |
|         |       | a.         | <b>a</b> . | ē.         |       | 60*        | .0         | .33        | •     | .2    | .33   | .39        | **    | 22            | .21         | 1.99  |
|         |       | 8.         | <b>a</b> . | 8.         |       | .12        | .15        | er.        | •     | .22   | .28   | .10        | 7.    | 8.            | .12         | 1.30  |
| 3 6     |       | a.         | 9.         | .10        |       | .10        | .25        | 64.        | •     | 64.   | 64.   | .33        | ``    |               | .23         | 2.56  |
|         |       | 8.         | .10        | 77.        |       | .39        | <b>3</b> . | .61        | •     | .55   | .51   | 04.        | **    |               | .16         | 3.77  |
| 3 3     |       | 60.        | 60•        | .39        |       | ₹5         | <b>6</b> . | <b>š</b> . | •     |       | 69.   | .52        | •     | 8             | .25         | 5.51  |
| 3 8     |       | 8.         | .33        | â          |       | # <b>.</b> | 1.02       | 1.36       | 1.    |       | 96.   | .57        | **    |               | .16         | 7.63  |
| 3 8     |       | 04.        | 0          | 8.         |       | 12         | 1.65       | 1.42       | 1.    |       | 96•   | 6#.        | e.,   |               | 23          | 9.40  |
| 3 8     |       | .75        | • 60       | 1.15       |       | 1.62       | 1.68       | 1.84       | 1     | 1.71  | 1.02  | .57        | ``}   |               | .15         | 11.34 |
|         |       | .72        | .78        | 1.36       |       | 1.83       | 2,29       | 2.33       | 1.    |       | .85   | 9#         | 7     |               | <b>ET</b> . | 12.42 |
| 3 8     |       | s.         | .87        | 1,39       |       | 2.02       | 2.18       | 1.92       | 1.    | 1.15  | .61   | 6 <b>*</b> | 7     |               | .15         | 11.63 |
| 3 3     |       | •          | 1.8        | 1,33       |       | 1.56       | 1.80       | 1.65       | ~     | 88    | .67   | 94.        |       | er.           | ē.          | 10.19 |
| 3 3     |       | <b>6</b> . | 8          | 66.        |       | 1.44       | 1,38       | 1.29       |       | *     | .37   | 04.        | •     |               | 8.          | 8.67  |
|         |       | .72        | .57        | .73        |       | 1.71       | .87        | .72        | •     | .51   | .28   | .22        | •     |               | ē.          | 5.99  |
| • 00°00 | 4     | .17        | .75        | 1.18       |       | 1.45       | 1,33       | .87        | •     | 39    | .22   | 60.        | 7     |               | <b>a</b> .  | 7.50  |

100.00

1.93

2.48

5.52

8.20

12.05

15.91

16.12

14,38

10.45

6.47

1966 - U. S. ARMY ANTHROPOMETRY SURVEY VERTICAL TRUNK CIRCUMFERENCE VS CHEST BREADTH

|                 |       |       |                 |             | VERTICAL   | TKUNK C | VERTICAL INUNE CINCUMPERENCE VS CHEST BREADIN | CE VS CHES | SI BALADIR |            |       |     |            |        |
|-----------------|-------|-------|-----------------|-------------|------------|---------|---|------------|------------|------------|-------|-----|------------|--------|
|                 | 10.00 | 10.50 | 11.00           | 11.00 11.50 |            | 12.00   | 12.50   | 13.00      | 13.50      | 14.00      | 14.50 |     | 15.06      |        |
| ;               |       | 8     | 8               | 00.         | <b>5</b> . | .10     | 54.   |            | 34         | 94.        | .22   | •19 | .18        | 1.99   |
| + 5.57<br>6 5 5 |       | 8     | 8.              | 8.          | ಕ್ಕ        | .25     | 36.   |            | .19        | .24        | .16   | 8.  | <b>a</b> . | 1,30   |
| • 60.17         |       | 8     | 00.             | ۶.          | .21        | .57     | 19.   |            | .55        | .37        | .21   | 8.  | .00        | 2.65   |
| + 00.07         |       | 8     | š.              | 60.         | .22        | 8.      | ð,  |            | .79        | 64.        | .18   | ä   | š.         | 3.77   |
| • 5             |       | 8     | 90,             | ₹.          | .75        | 1.68    | 1,45  |            | .75        | .39        | .16   | 8   | 00.        | 5.51   |
| \$ 5<br>\$ \$   |       | ន     | a.              | <b>š</b> .  | 1.20       | 2.02    | 2.08  |            | 1.14       | .28        | .21   | 00. | 8          | 7.63   |
|                 |       | ą.    | .28             | .82         | 2.16       | 2.59    | 2.11  |            | 06.        | .36        | .12   | 5   | 8          | 04.6   |
| 8 8             |       | .10   | .51             | 1.72        | 3.19       | 2.90    | 1.84  |            | .79        | .21        | .07   | 8.  | 8.         | 11.34  |
|                 |       | 8     | <b>3</b> 0.     | 2.26        | 3.13       | 3.47    | 1.92  |            | .52        | .13        | 90•   | 8.  | 8          | 12.42  |
| 3 3             |       | .22   | 98              | 2.11        | 3.50       | 3.14    | 1,32  |            | .28        | .12        | 8.    | 00. | ਰ.         | n.63   |
| 3 3             |       | .16   | 1.12            | 2.45        | 2.84       | 2.27    | \$.   |            | .36        | 8.         | 00.   | 00. | 8          | 10.19  |
| 6.50            |       | .39   | 1.02            | 2.48        | 2.48       | 1,65    | .52   |            | ,10        | 00•        | • 00  | 8.  | 00.        | 8.67   |
| 8 9             |       | ¥6.   | ξÝ              | 1.86        | 1.78       | .78     | .21   |            | .07        | ю <b>.</b> | 00.   | 8.  | 00.        | 5.99   |
| 59.00 +         |       | .79   | 2.16            | 2,53        | 1.27       | ŝ       | .12   |            | 00.        | · •        | 00•   | 8   | 8.         | 7.50   |
|                 |       | 2.16  | 2,16 7,98 17,18 | 17.18       | 22,79      | 23.00   | 24.89   |            | 6.81       | 3.11       | 1.44  | .39 | .25        | 100.00 |

Appendix C
Bivariates of Proposed Fitting Criteria For
Three-Size System

1966 - U. S. ARMY ANTRHOPOMETRY SURVEY VERTICAL TRUNK CIRCUMFERENCE VS CHEST CIRCUMFEREN

1966 - U. S. ARMY ANTHROPONETRY SURVEY VERTICAL TRUNK CIRCUMFERENCE VS WAIST CIRCUMFERENCE

| % •           | <b>58.</b> 00 | 30.00    | 32.00        | 00° †C 00 |       | 36.00    | 38.00      | 00°¢       | <b>#2.</b> 00<br>+ | 00.**      | <b>4 4 6 9</b> | •          |        |
|---------------|---------------|----------|--------------|-----------|-------|----------|------------|------------|--------------------|------------|----------------|------------|--------|
|               | 8.            | <b>ਰ</b> | 8            | ٠٠.       | u.    |          | 8          | 67.        | 04.                | .19        | .10            | 8          | 1.99   |
|               | 8.            | 8        | .12          | .22       | .15   | e        | .24        | 34.        | .12                | 60.        | <b>8</b> .     | 8          | 1.30   |
|               | 8.            | 5        | ĸ            | 3.        | 99•   | -        | .52        | .28        | .21                | .00        | 8.             | <b>a</b> . | 2.66   |
|               | ន             | 60•      | .51          | .79       | 1.02  | <u>0</u> | .60        | .#3        | *5*                | ₫.         | 8.             | a.         | 3.17   |
|               | 01.           | .30      | .97          | 1,57      | 1,35  | 1        | .75        | <b>.34</b> | .07                | 8.         | %              | 8          | 5.51   |
|               | .10           |          | Z 1.88       | 2,08      | 1,38  |          | 88.        | .21        | .12                | .01        | 00.            | 8          | 7.63   |
|               | .22           | 1.30     | ة.<br>ج<br>ا | 2.44      | 1.5   |          | <b>3</b> . | .21        | 60°                | <b>a</b> . | 00.            | 8          | 04.6   |
|               | .39           | 2.26     | 6.           | 2.63      | 1.23  |          | .55        | .15        | 8.                 | 8.         | %              | 8          | т:з    |
|               | s,            | 3.56     | ر ا<br>1.19  | 2.41      | 1.02  |          | .33        | 8          | <b>%</b>           | .01        | 8.             | 8          | 12.42  |
|               | .80           | 3.56     | *.10         | 2.10      | 19:   | •        | .22        | 8.         | 8.                 | 00.        | 8.             | 8          | 11.63  |
| _ا_           | 1.17          | 8.8      | 3.01         | 1.30      | .52   |          | .15        | <b>%</b>   | 00•                | 00.        | 00.            | 8          | 10.19  |
| <b>7</b>      | 1.40          | 3.56     | 2.66         | 91.       | .19   |          | 8.         | %          | 00.                | 00.        | %.             | 8          | 8.67   |
| <b>&gt;</b> H | 1.29          | 2.63     | 1.56         | .39       | .12   |          | %          | 8.         | • 00               | 8.         | • 00           | 8          | 5.99   |
| S             | 2.8           | 3.10     | 1.09         | .21       | .12   |          | 8          | 00.        | 8.                 | 00.        | 8.             | 8          | 7.50   |
|               |               | 1        |              |           |       |          |            |            |                    |            |                |            |        |
|               | 25.0          | 25.28    | 27.60        | 17.57     | 10.18 | S        | 5.27       | 2.48       | 1.29               | • 52       | .15            | S.         | 100.00 |

1966 - U. S. ARMY ANTHROPOMETRY SURVEY CHEST CIRCUMFERENCE VS WAIST CIRCUMFERENCE

|                |       |       |       |                    |       | Ü            | HEST CIRC |       | CHEST CIRCUMFERENCE VS WAIST CIRCUMFERENCE | IST CIRCUM | ERENCE     |      |      |            |            |        |
|----------------|-------|-------|-------|--------------------|-------|--------------|-----------|-------|--|------------|------------|------|------|------------|------------|--------|
|                | 26.00 | 28.00 |       | 30.00              | 32.00 | 34.00        |           | 36.00 | 38.07                                      | 00.04      | 42.00      |      | 90.+ | *6.00<br>+ | •          |        |
| ;              |       | 8.    | 00.   | 00.                |       | 00.          | 00.       |       | 00.  | а <b>.</b> | <b>ة</b> . | 90.  | •    | 8          | ē.         | .18    |
| <b>47.50</b> + |       | 00.   | 8     | 60.                |       | · 00         | ъ.        | C     | • 00                                       | ಕ          | 60.        | .15  | •    | 5          | 8.         | £43    |
| \$ 06°0        |       | 8.    | 8     | 00.                |       | 8.           | 01.       | N     | .22  | .31        | .37        | £1.  | •    | 5          | 8          | 1.23   |
| + 00.5         |       | 00.   | 8     | 8.                 |       | £1.          | 09.       | 70    | 1.14                                       | .81        | 64.        | .13  | •    | <b>a</b> . | <b>a</b> . | 3.37   |
| + 00.44        |       | .01   | .15   | .81                |       | 2.32         | 3.02      | ••    | 2.39                                       | ₹.         | .30        | 93   | •    | 8.         | 8.         | 86     |
| + 70.00        |       | .12   | 1.58  | <b>Q.</b> 6.119    |       | 7.42         | 4.79      |       | 1.29                                       | ,24        | 00.        | ۵.   |      | 8          | 18         | 21.73  |
| 37.58          |       | 1,05  | 9.46  | <b>25</b><br>14.25 |       | <b>6.</b> 64 | 1.47      |       | .10  | ،10        | 00.        | • 00 | ·    | 8.         | 00.        | 32.07  |
| + 2000         |       | ¥.06  | 12.56 | 5.85               |       | 8.           | .15       |       | <b>8</b> .                                 | .01        | 00•        | %    | •    | 8          | 8.         | 23.59  |
|                |       | 3,82  | 2.39  | 87.                |       | 60•          | ٠.        |       | 8  | 00.        | 00.        | 00.  | ·    | 8.         | %          | 6.82   |
|                | ŦO    | 64,   | Š.    | 00.                |       | 80.          | • 0       |       | 00.  | 00.        | 00.        | 00.  | ·    | 8          | 00.        | • 55   |
|                | Н     | ъ.    | 8     | .00                |       | 00.          | 00.       |       | 00.  | ٠,00       | 00•        | 000  | ·    | 8.         | 8.         | a.     |
| 25.50 +        | S     | 8     | 00.   | 00.                |       | 8.           | 00,       |       | 00.  | 00.        | 00.        | 00•  | •    | 8          | 8          | 8      |
|                |       | 3,59  | 25.28 | 27.60              |       | 17.57        | 10.18     |       | 5.27                                       | 2.48       | 1.27       | .52  |      | .15        | 60         | 100.00 |

Appendix D

Bivariates of Proposed Fitting Criteria For Four Size System

|       |      |      |      |            |      |            | T TUCOUIT | TENTION TOWN CINCULATIONS OF STREET | NEO ISTUI  | COURT ENGINEE | ,    |      |       |    |       |
|-------|------|------|------|------------|------|------------|-----------|-------------------------------------|------------|---------------|------|------|-------|----|-------|
| 23.55 | 32.5 | 33.5 | 34.5 | 36.5       | 36.5 | 37.5       | 38.5      | 39.5                                | 40.5       | 41.5          | 42.5 | 43.5 | 5° nh |    |       |
|       | ė.   | •    | o.   | •          | •    | °.         | ۵.        | ٠.                                  | ۲:         | .2            | י:   | ٠:   | ۲.    | ۳. | 171   |
| 3 5   | ٥.   | ó    | ٥.   | °.         | •    | o,         | 3.        | ۲.                                  | ۲.         | .2            | ••   | ۲.   | 7     | 7. | 6.    |
|       | e,   | •    | ٥.   | ٥.         | 0.   | 0.         | ~         | 7.                                  | 7          | • 5           | 7.   | 7    | 7     | Ţ. | 1.3   |
| 3 6   | o.   | °.   | ۰.   | o.         | ٠.   | 2,         | e,        | 'n                                  | €.         | <b>4</b> ,    | • 5  | • 5  | .2    | r. | 2.7   |
| 3 8   | o.   | °.   | •    | 7.         | .2   | <b>.</b> 7 | s.        | 9.                                  | œ.         | s.            | •5   | .2   | ۲.    | T. | 3.8   |
| 3     | o.   | ۰.   | ۲.   | •2         | 9.   | 8.         | 1.1       | 1.0                                 | φ.         | ø.            | ۴,   | .2   | r.    | ۰. | 5.5   |
| 3 8   | ė.   | o,   | 3,   | s,         | 1.0  | 6.4        | 1.2       | 1.4                                 | 6.         | ĸ,            | ۴.   | ۲.   | •     | 7  | 7.6   |
|       | -:   | 7    | e.   | æ          | 1.8  | 1.0        | 1.5       | 1.3                                 | æ          | 3.            | •5   | ۲:   | ۲.    | •  | 4.6   |
|       | •    | e.   | ۲,   | 9 7        | 7.0  | 2.1        | 1.8       | 1.3                                 | 8.         | .3            | .2   | °.   | ۰.    | ٥. | п.3   |
|       | 7    | 9.   | 1,3  | 1.9        | 2.6  | 2.2        | 1.6       | 1.1                                 | <b>a</b> , | .3            | 7.   | ٥.   | 6     | •  | 12.4  |
|       | 7:   | \$.  | 1.2  | 1.9        | 2.7  | 2.3        | 1.3       | σ.                                  | ₹.         | 7.            | °.   | °.   | o.    | ٥. | 11.6  |
| 8 8   | ę.   | ę    | 1.3  | 2.0        | 2.1  | 7:         | 1.1       |                                     | <b>4</b> , | 7             | ٥.   | 0.   | ۰.    | ۰. | 10.2  |
| 3 5   | ς,   | •    | 1.2  | 2.0        | 1.9  | 1.1        | «.        | e.                                  | ٠:         | ۲.            | •    | °.   | •     | ٥. | 8.7   |
|       | •    | ń    | 4    | N. L       | 7.2  | 9          | ۴.        | .2                                  | ٦.         | ٠:            | •    | °.   | 0.    | ٥. | 6.0   |
|       | e,   | á    | ó    | æ          | ø.   | ٤,         | Ţ.        | 7.                                  | °.         | °.            | o.   | •    | ٥.    | •  | 3.6   |
| 5     | 7.   | ů    | s.   | <b>3</b> . | е.   | <u>-</u>   | .1        | .1                                  | 0.         | °.            | °.   | ٥.   | ٥.    | o. | 2.0   |
|       | *,   | ٠,   | v,   | eć         | .2   | 7          | 0,        | ٥.                                  | ٥.         | 0.            | 0.   | ٥.   | •     | ٥. | 1.9   |
| }     |      |      |      |            |      | 1          |           |                                     |            |               |      |      |       |    |       |
|       | 2.3  |      | 9.7  | 13.9       | 17.2 | 8,41       | 12.1      | 7.6                                 | 0.9        | 0.4           | 2.1  | 1.3  | 7.0   | σ. | 100.0 |

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| 26.0        | 27.0   | 28.0   | 29.0 | 30.0 | 31.5   | 32.0 | 31.5     | 34.0 | 35.0 | 36.0 | 37.0   | 38.0 | 39.0    | 0.05       | 41.0 | 42.0       | •  |      |
|-------------|--------|--------|------|------|--------|------|----------|------|------|------|--------|------|---------|------------|------|------------|----|------|
| •           | •      | •<br>• | °    | e.   | ,<br>o | o.   | ų        | · .  | ٥.   | •    | ,<br>o | ٠.   | ,<br>c. | · -:       | · -: | · -:       | *  | 6.   |
| 000         | •      | o.     | ٥.   | •    | ٥.     | o.   | o.       | 5.   | ¢,   | 7.   | a,     | ۲.   | ~       | * <u> </u> | 7.   | .2         | τ. | 1.0  |
| + 05.50     | ٥.     | ٥.     | o.   | o.   | o.     | o.   | °.       | ò    | ۲.   | ۲.   | r;     | £.   | ŗ       | ۲.         | •5   | <b>:</b> : | ۲. | 1.3  |
|             | 0.     | ۰.     | °.   | ė.   | •      | င့   | ů,       | ٦:   | ~    | €.   | *.     | ۴,   | 7.      | -5         | =    | <b>-</b> ; | 7  | 2.1  |
| • 06.14     | •      | •      | •    | ٥.   | ۲.     | 7    | .2       | r.   | ₹.   | ۲.   | s,     | ų,   | 4       | ۲.         | 7    | ۲.         | ٥. | 0.   |
|             | o.     | o.     | •    | ٦.   | 7.     | ₹.   | <b>.</b> | 1.0  | 1.0  | ø,   |        | សុ   | ٠.      | ۲.         | ٥.   | ٥.         | c. | 6.0  |
| ÷ 06.65     | •      | ٥.     | ۲.   | 7,   | ۲.     | 1,3  | 3.8      | 1.7  | 2,5  | 1.1  | 9      | e.   | ٦.      | 7          | 0.   | 0.         | •  | 9.7  |
| )<br>)<br>1 | 0.     | 7      |      | 1.0  | 1.8    | 2.3  | 2.3      | 1.5  | 1.5  | ۲.   | ۳,     | ۲.   | 7       | •          | ¢.   | 0.         | ٥. | 12.1 |
|             | 7      | ~      | e.   | 2.0  | 2.8    | 3.5  | 2.6      | 1,6  | e.   | .3   | 7.     | o.   | ي.      | °.         | ė.   | o.         | •  | 14.8 |
|             | 7.     | ۲.     | 1.7  | 3.9  | 4.2    | 3.7  | 1.8      | ۲.   | E,   | 7    | o.     | o,   | ٥.      | ٥.         | 0.   | c.         | 0  | 17.2 |
|             | e,     | 1.5    | 2.7  | 0.*  | 2.9    | 1.6  | ĉ        | .2   | τ.   | •    | o.     | •    | •       | •          | ٥.   | °.         | 0. | 13.9 |
| 26.50       | ٠.     | 1.6    | 3.2  | 2.6  | 1.0    | *    | 7        | °.   | ٥.   | ۰.   | °.     | ٥.   | ٥.      | ٥.         | ٥.   | ٥.         | 0. | 4.5  |
|             | œ.     | 1.8    | 1.1  | æ    | m,     | 7.   | 7.       | ٥.   | o.   | •    | ٥.     | ė.   | •       | °.         | o,   | o.         | °, | 5.1  |
| 00.70       | ٠<br>• | •      | ₹.   | 7.   | 7.     | °.   | •        | •    | 0.   | °.   | o.     | •    | •       | o.         | 0.   | 0.         | •  | 2.3  |
| 31.50 +     |        |        |      |      |        |      |          |      |      |      |        |      |         |            |      |            |    |      |

.8 100.0

4.2

6.7 10.4 15.9 14.0 13.6 10.2

1966 - U. S. ARMY ANTHROPOMETRY SURVEY MENTER THE THEM CITCHERED TO MAIST CIRCUMSTREME

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THE COMPANY OF THE CONTROL OF THE CO

|                 |     |     |          |      |      |      | VERT I   | VERTICAL TRUNK |      | CIRCUNTERFINE VS MAIST CIRCUMFERENCE | VS WAI     | ST CIRC    | UNITERED | ZE<br>ZE    |      |      |            |            |
|-----------------|-----|-----|----------|------|------|------|----------|----------------|------|--------------------------------------|------------|------------|----------|-------------|------|------|------------|------------|
| *               | 3.0 | 8.0 | 29.6     | 30.0 | 31.0 | 32.0 | 33.0     | 34.0           | 35.0 | 36.0                                 | 37.0       | 38.0       | 39.0     | 0.04        | 41.0 | #2.0 | •          |            |
|                 | •   | o.  | ٥.       | •    | ۰.   | ő,   | °.       | o,             | ٥.   | ٦.                                   | ۲.         | .2         | 7.       | ٦.          | 7.   | ۲.   | e.         | 1.1        |
| 73.00 ÷         | ę.  | e.  | e.       | ۰.   | o.   | o.   | ٥.       | ٥.             | ۲.   | ۲.                                   | r.         | r.         | ۲.       | .2          | ד.   | ٠,   | ٦.         | 6          |
| 72.00 +         | o,  | o.  | ć        | •    | o.   | ~    | 7.       | r.             | 7.   |                                      | ٠,         | r.         | ~        | 7:          | 7.   | ۰.   | 7          | 1.3        |
| 71.00 +         | •   | ó   | ٥.       | •    | ۲.   | ~    | .2       | 3.             | ۴.   | 3,                                   | ۴.         | .2         | 7.       | ~           | ٠:   | ۲.   | 7.         | 2.7        |
| 70,00 ÷         | ó   | o.  | •        | 7.   | .2   | r.   | ٠,       | ۳,             | s.   | s.                                   | e.         | ۳ <b>.</b> | ~        | • 5         | .2   | 7.   | 7.         | 3.8        |
| ÷ 28.88         | •   | 7   | ٦,       | .2   | 4.   | s.   | ۴.       | æ              | ٠.   | .,                                   | <b>3</b> . | ₹.         | 5.       | Ţ.          | •    | ٥.   | °.         | 5.5        |
| 3<br>3          | o.  | 7   | .2       | 9.   | 80   | 1.2  | 1.1      | 1.0            | 6.   | ĸ,                                   | χŷ         | ۴.         | ۲.       | ۲.          | ۲.   | •    | °.         | 7.6        |
| ÷ 65.           | °.  | ۲.  | e,       | 1.0  | 1.2  | 9.1  | 7.1      | 1.0            | ∞.   | ٠,                                   | ۴.         | .2         |          | 7.          | 0.   | r.   | ۰.         | <b>#</b> . |
| •<br>8.3        | 7   | ų.  | ø.       | 3.6  | 7.0  | 2.1  | 1.5      | 1.2            | e.   | 7.                                   | 6.         | .2         | ٠.       | o.          | o.   | •    | o.         | 11.3       |
| • 2.00 ·        | .2  | ٦,  | 1.3      | 2.2  | 2.1  | 2.1  | 2.5      | ø,             | 9    | ₹.                                   | •5         | 7          | ٥.       | •           | •    | ٥.   | 0.         | 12.4       |
| 8.3             | .2  | r   | 1.5      | 2.1  | 2.2  | 1.9  | 1.3      | •              | a,   | .2                                   | .2         | ٥.         | •        | ۰.          | ۰.   | 4)   | •          | 11.6       |
| <b>8</b> .      | ų   | e.  | 1.8      | 2.2  | 1,0  | 1.3  | 1.0      | £.             | 3.   | ۲.                                   | ۲.         | 7.         | ٥.       | °.          | c.   | ć.   | •          | 10.2       |
| <b>6</b> 2.00 + | 4.  | 1.1 | 1.5      | 2.0  | 1.5  | 3.2  | νį       | €.             | 7.   | ۲.                                   | ٥.         | 0.         | ć.       | ي.          | ٥.   | •    | •          | 7.0        |
| 3.3             | ò   | ٠.  | 1.3      | 1.3  | 1.0  | .9   | .2       | 7              | 7.   | o.                                   | 0.         | ۰.         | o.       | °.          | •    | •    | o.         | 6.0        |
| \$ 00°00        | œ.  | œ.  | <b>5</b> | æ    | νņ.  | .2   | <b>∹</b> | o.             | 7.   | •                                    | ۰.         | ٥.         | 0.       | •           | ٥.   | ۰.   | o,         | 3.6        |
| ÷ 08° 69        | 6   | ñ,  | *,       | *.   | ٦.   |      | 4.       | o.             | o.   | o.                                   | °          | 0.         | 5        | <b>1</b> º. | •    | ۰.   | o,         | 2.0        |
| 57.98 +         | ĸ.  | ٠.  | .2       | ú    | -    | o.   | •        | °.             | o.   | •                                    | ¢.         | •          | •        | 0.          | •    | ¢.   | ઙ          | 1.9        |
|                 |     |     | 0.44     | 1    | i    | 13.6 | 10.2     | 7.4            | 5.9  | 4.2                                  | 2.9        | 2.4        | 1.4      | 1.1         | e.   | s.   | <u>ئ</u> د | 130.0      |

5.9

7.4

10.4 14.9 14.0 13.6 10.2

6.7

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